

Computer Methods of Analysis of Offshore Structures
Prof. Srinivasan Chandrasekaran
Department of Ocean Engineering
Indian Institute of Technology, Madras

Module - 02
Lecture - 13
Dynamic Analysis - 2 (Part - 2)

I can now write the control equations for finding the mode shape and frequency.

(Refer Slide Time: 00:25)

The slide contains the following equations:

$$x_1 = \alpha_{11} \omega_m^2 x_1 + \alpha_{12} \omega_m^2 x_2 + \alpha_{13} \omega_m^2 x_3$$

$$x_2 = \alpha_{21} \omega_m^2 x_1 + \alpha_{22} \omega_m^2 x_2 + \alpha_{23} \omega_m^2 x_3$$

$$x_3 = \alpha_{31} \omega_m^2 x_1 + \alpha_{32} \omega_m^2 x_2 + \alpha_{33} \omega_m^2 x_3$$

$$\begin{Bmatrix} x_1 \\ x_2 \\ x_3 \end{Bmatrix} = \frac{\omega_m^2}{k} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{Bmatrix} x_1 \\ x_2 \\ x_3 \end{Bmatrix} = 1$$

$x_1 \times 2 \times 3$ is actually equal to α_{11} , α_{21} , α_{31} plus α_{12} , α_{22} , α_{32} , α_{13} , α_{23} and α_{33} that is first row first column first row second column first row third column and so on, multiply $\omega_m^2 \times 1$, $\omega_m^2 \times 1$, $\omega_m^2 \times 1$. So, this becomes $\omega_m^2 \times 2$, $\omega_m^2 \times 2$, $\omega_m^2 \times 3$; $\omega_m^2 \times 3$.

I can now write this in a matrix form $x_1 \times 2 \times 3$ as ω_m^2 by k of $1 \ 1 \ 1$, $1 \ 2 \ 2$, $1 \ 2 \ 3$ that is my α matrix with m . I will multiply it by x_1 , x_2 , x_3 - equation 1. Now you can see in this equation the vector x_1 , x_2 , x_3 are present both in left hand side and right hand side. So, the scheme becomes iterative I assume the value of this vector substitute and see what value I am getting back if the assumed value and the obtained value are same then the solution is converged.

(Refer Slide Time: 02:28)

The slide shows three iterations of a power method calculation for a mode shape. The equations are as follows:

$$\begin{Bmatrix} 1 \\ 1 \\ 1 \end{Bmatrix} = \frac{\omega_m^2}{k} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{Bmatrix} 1 \\ 1 \\ 1 \end{Bmatrix} = \frac{\omega_m^2}{k} (3) \begin{Bmatrix} 1 \\ 1.67 \\ 2.0 \end{Bmatrix}$$

$$\begin{Bmatrix} 1.67 \\ 2.0 \end{Bmatrix} = \frac{\omega_m^2}{k} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{Bmatrix} 1 \\ 1.67 \\ 2.0 \end{Bmatrix} = \frac{\omega_m^2}{k} (4.67) \begin{Bmatrix} 1 \\ 1.79 \\ 2.21 \end{Bmatrix}$$

$$\begin{Bmatrix} 1.79 \\ 2.21 \end{Bmatrix} = \frac{\omega_m^2}{k} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{Bmatrix} 1 \\ 1.79 \\ 2.21 \end{Bmatrix}$$

Let us start with the first mode shape zero crossing let us take it as all 1 1 1 which will be omega square m by k times of 1 1 1, 1 2 2, 1 2 3 of 11 1 let us multiply and see what happens. So, omega square 1 m by k I take a multiply 3 out if we do that I get a vector as 1, 1.67 and 2.0. I started with 1 1 1, I got 1, 1.67, 2 so no convergence let us start the second iteration with 1, 1.67 and 2.0 as omega square m by k 1 1 1, 1 2 2, 1 2 3 multiplied with 1, 1.67 2.0 which gives me omega square m by k 4 0.67 is the multiplier I get 1, 1.79, 2.21.

Again this converges not happened let us take the next iteration 1, 1.79, 2.21 is omega square m by k 1 1 1, 1 2 2, 1 2 3 of 1, 1.79, 2.21 which becomes omega square m by k. Now the multiplier is 5, if I do that I get this value as 1, 1.8, 2.24. I do one more iteration 1, 1.8, 2.24 is equal to omega square m by k 1 1 1, 1 2 2, 1 2 3 multiplied by 1, 1.8, 2.24 which will give me omega square m by k the multiplies 5.04 and I get a vector as 1, 1.801 and 2.25.

(Refer Slide Time: 04:54)

The slide shows the following equations and notes:

$$\begin{Bmatrix} 1 \\ 1.8 \\ 2.24 \end{Bmatrix} = \frac{\omega_m^2}{k} \begin{bmatrix} 1 & 1 & 1 \\ 1 & 2 & 2 \\ 1 & 2 & 3 \end{bmatrix} \begin{Bmatrix} 1 \\ 1.8 \\ 2.24 \end{Bmatrix} = \frac{\omega_m^2}{k} (5.04) \begin{Bmatrix} 1 \\ 1.801 \\ 2.25 \end{Bmatrix}$$

$$1 = \frac{\omega_m^2}{k} (5.04) \quad (1)$$

$$\omega_1 = 0.445 \sqrt{k/m}$$

$$\phi_1 = \begin{Bmatrix} 1 \\ 1.801 \\ 2.25 \end{Bmatrix}$$

First/fundamental frequency
Zero crossing - mode shape

So, they are more or less converging once they are converging let us write down the equality 1 is equal to omega square m by k 5.04 of 1 which implies that omega is actually equal to 0.445 square root of k by m and the corresponding mode shape is 1, 1.801, 2.25. So, this is my first or fundamental frequency. Why fundamental frequency? I think you will have to guess this, this is because the mode shapes has zero crossing. So, it is the first mode shape. So, I should say now omega 1 and phi 1.

So, I can also obtain the fundamental frequency and mode shape using influence coefficient method as omega 1 and phi 1.

(Refer Slide Time: 06:34)

Higher modes - using the principle of orthogonality

$$\begin{Bmatrix} A_1 \\ B_1 \\ C_1 \end{Bmatrix} \text{ 1st mode} \quad \begin{Bmatrix} A_2 \\ B_2 \\ C_2 \end{Bmatrix} \text{ 2nd mode}$$

Let modes be orthogonal.

$$m_1 A_1 A_2 + m_2 B_1 B_2 + m_3 C_1 C_2 = 0$$

$$(m_1) A_2 + (m_2) (1.801) B_2 + (m_3) (2.25) C_2 = 0$$

Let $C_2 = C_2$
 $B_2 = B_2$
 $A_2 = f(C_2, B_2)$

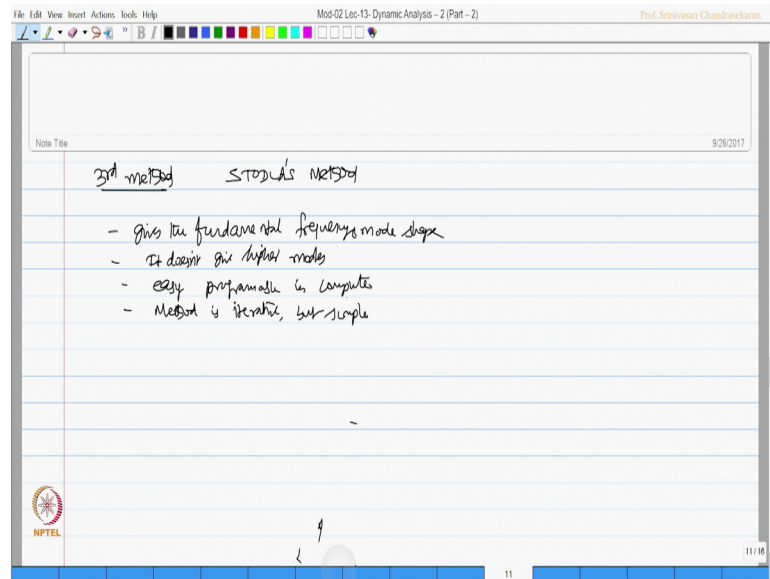
NPTEL higher modes dynamics

I can also obtain the higher modes using the principle of orthogonality. So, I can also get the higher modes using the principle of orthogonality, I will quickly explain you let us say A_1, B_1, C_1 is the first mode vector and let A_2, B_2, C_2 be the second mode vector in other case is going to be 1, 1.801 and 2.25. Let us do not know the second mode take it as A_2, B_2 and C_2 .

So, let modes be orthogonal if they are orthogonal then $m_1 A_1 A_2$ plus $m_2 B_1 B_2$ plus $m_3 C_1 C_2$ will be 0. So, m in our case is 1 value a 1 in our case is 1 and a 2 we do not know plus m_2 now cases m and 1.801 and B_2 plus m_3 2.25 and C_2 is set to 0. So, I will get an equation in $A_2 B_2 C_2$. So, let C_2 to be C_2, B_2 be B_2 and express A_2 as a function of C_2 and B_2 and then apply the algorithmic principle and try to obtain the higher modes. I am not solving the higher modes in this particular lecture you can please refer to the NPTEL notes on dynamics or the textbooks which you have referred in the last lecture on dynamics written by me and you can compute the higher modes.

So, now we have learned the second method that is influence coefficient method which gives me the value of fundamental frequencies and mode shapes and higher modes as well. So, now, let us look at the third method which is given by **Stodola**.

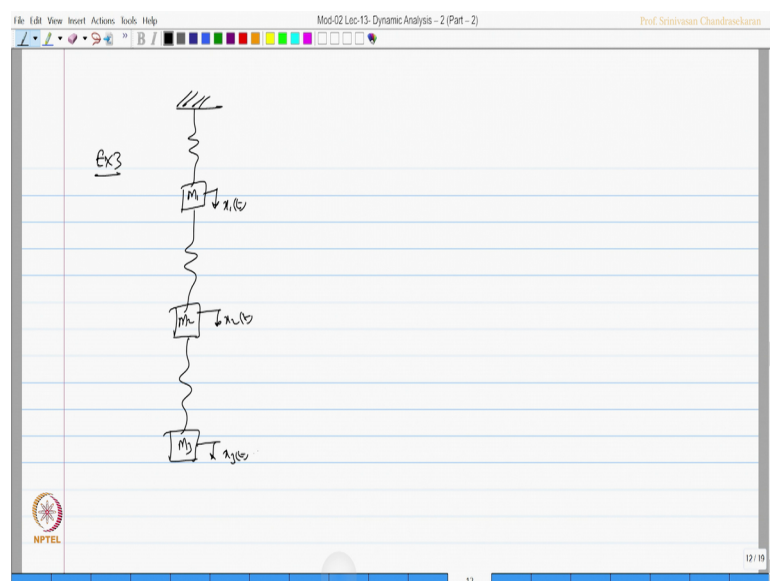
(Refer Slide Time: 09:08)



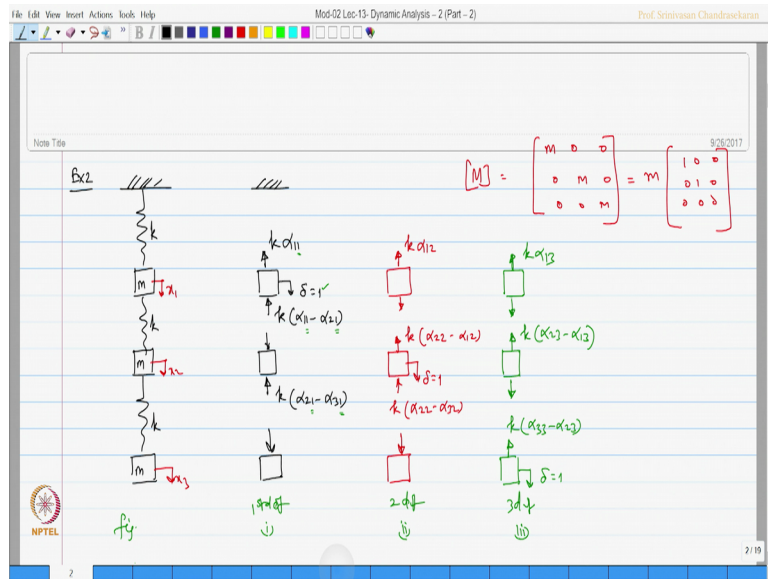
So, **Stodola** method gives the fundamental frequency and mode shape it does not give higher modes the method is easily programmable by computer though the method is iterative, but simple.

Let us take the same example and solve. So, the example 3, but similar to example 2 that is m_1, m_2, m_3 , this is x_1 of t , this is x_2 of t , this is x_3 of t which is same as this example, same as this example provided m_s and k_s are well defined in the same fashion.

(Refer Slide Time: 10:40)



(Refer Slide Time: 11:06)



So, let $m_1 = m_2 = m_3 = m$, similarly this is k_1 this is k_2 this is k_3 let $k_1 = k_2 = k_3 = k$. So, let us try to solve this problem using Stodla's method. So, let us assume deflection say $k_1 m_1$, $k_2 m_2$ and $k_3 m_3$. Let us say the assumed deflection is at the mass points 1, 1 and 1.

The inertia force could be $m_1 \omega^2 \delta_1$ and this is going to be $m_2 \omega^2 \delta_2$ deflection, $m_3 \omega^2 \delta_3$ deflection.

(Refer Slide Time: 12:27)

	k_1	m_1	k_2	m_2	k_3	m_3
Assumed deflection		$m_1 \omega^2 \delta_1$		$m_2 \omega^2 \delta_2$		$m_3 \omega^2 \delta_3$
Spring force	$3m\omega^2$		$2m\omega^2$		$m\omega^2$	
Spring deflection	$\frac{3m\omega^2}{k_1}$		$\frac{2m\omega^2}{k_2}$		$\frac{m\omega^2}{k_3}$	
Calculated deflection		$3\omega^2$		$5\omega^2$		$6\omega^2$
deflect		$1 \omega^2$		$1.67 \omega^2$		$2 \omega^2$
$F_2 (m)$		ω^2		$1.67\omega^2$		$2\omega^2$
Spring force (m)	$4.67\omega^2$		$3.67\omega^2$		$2\omega^2$	
Spring def (m/k)	$4.67\omega^2$		$3.67\omega^2$		$2\omega^2$	
Calculated δ (m)		$4.67\omega^2$		$8.34\omega^2$		$10.34\omega^2$
		1.0		1.79		2.21

Now, I want to compute the spring force the spring force for k_3 that is the spring force for k_3 will be actually equal to $m \omega^2$ and for k_2 it will be $2 m \omega^2$ it is because m_2 and m_1 are all equal to m , there is the reason. Similarly for k_1 it will be $3 m \omega^2$ I want to find the spring deflection, I divide this by k_1 so $3 m \omega^2$ square by k_1 , $m \omega^2$ square by k_2 , $m \omega^2$ square by k_3 .

So, now I want to compute the calculated deflection. So, I keep m and k out. So, I should say here this is going to be $3 \omega^2$ I should say k by m and $\phi \omega^2$ and $6 \omega^2$. So, now, we can find the ratio keep this as 1, keep this as 1 so this will become 1.67 and this will become 2. So, I started with 1, 1.67 and 2 so no convergence.

So, I will repeat the same case starting at 1, 1.67 and 2. So, I would say these are my deflections. So, this is the first iteration, deflection is 1, 1.67, 2 I calculate inertia force I take multiplier m out. So, this is going to be $2 \omega^2$, there is 1.67 ω^2 square this is ω^2 . I calculate the spring force again m out which is going to be $2 \omega^2$, $3 \times 0.67 \omega^2$, $4 \times 0.67 \omega^2$. I say spring deflection again I say it is m by k $4.67 \omega^2$, $3.67 \omega^2$, $2 \omega^2$. I get calculated deflection is m by k is going to be $4.67 \omega^2$, $8.34 \omega^2$ just sum them up and $10.34 \omega^2$. Now, I take a ratio take this as 1 this becomes 1.79 and this becomes 2.21. I started with 1, 1.67 and 2, but ended in 1; 1.79 and 2.21 again no convergence.

Let us do the third cycle assume deflection, which is let us say this is k_1 this is m_1 , this is k_2 this is m_2 , this is k_3 this is m_3 .

(Refer Slide Time: 17:34)

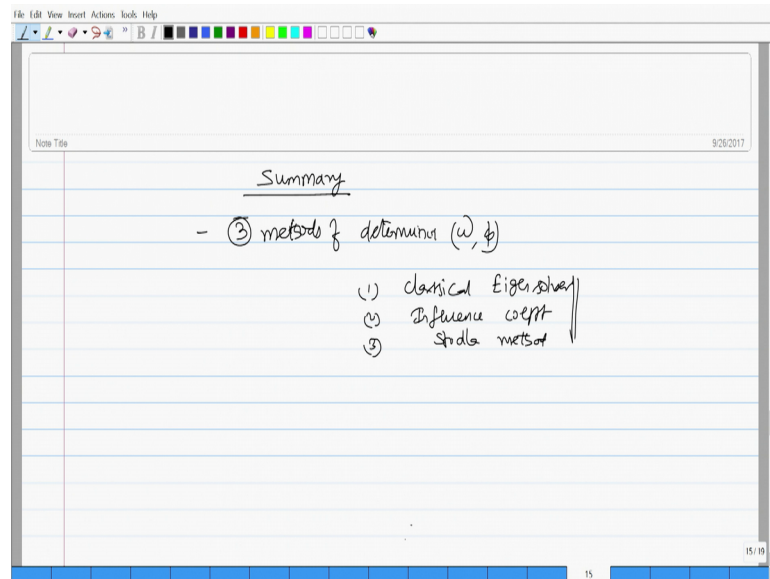
k_1 m_1 k_2 m_2 k_3 m_3
 Assumed defl 1 1.79 2.21
 Inertia force ($m\ddot{x}$) ω^2 $1.79\omega^2$ $2.21\omega^2$
 Spring force (F_s) $5\omega^2$ $4\omega^2$ $2.21\omega^2$
 Spring defn (x_s) $5\omega^2$ $4\omega^2$ $2.21\omega^2$
 Calculator def (x_c) 1.0 1.80 2.24
 $(1.0 + 1.8 + 2.24) = (5 + 9 + 11.21) \omega^2 (m/k)$
 $\omega = 0.447 \sqrt{k/m}$
 $\phi = \begin{Bmatrix} 1 \\ 1.80 \\ 2.24 \end{Bmatrix}$

So, assume deflections are 1, 1.79 and 2.21 that is what we are borrowed from the last iteration. So, the inertia force m out will be $2.21 \omega^2$, $1.79 \omega^2$ and ω^2 square. Spring force with m out will be $2.21 \omega^2$ which becomes $4.0 \omega^2$ which becomes $5 \omega^2$ as summation. Then I find spring deflection so divided by the stiffness, so it is going to be $5 \omega^2$, $4 \omega^2$ and $2.21 \omega^2$.

Now, I say calculator deflection I say this is going to be $5 \omega^2$. I get this at the mass points this is going to be $9 \omega^2$ and $11.21 \omega^2$. I now take a ratio say this is 1, this is 1.80 and this is 2.24. I believe that it has converged because the previous iteration the values were 1, 1.79 and 2.21; now it is 1, 1.8 and 2.24. Once it is converged we say that $1 + 1.8 + 2.24$ will be equal to $5 + 9 + 11.21 \omega^2 m/k$. So, if you are called I get ω as $0.447 \sqrt{k/m}$.

So, if you look at the results of influence coefficient method we got $0.445 \sqrt{k/m}$ and the mode shapes were 1, 1.801 and 2.25. Now we let us see what result do we get from here ω is 0.447 and the corresponding ϕ is 1, 1.80 and 2.24. Let us quickly compare these results 0.447 and this whereas this value is 0.445 and 1.8, 2.25. See very closely they are matching.

(Refer Slide Time: 20:49)



So, we learnt 3 methods in this lecture, we learned 3 methods of determining omega and phi that is a natural frequency and more shapes the methods are Classical Eigen solver method to Influence coefficient method, 3 **Stodola** method. All these are easily programmable we will be giving you also the computer methods of this and write the program and then solve the problem using the computer program and compare the results.

Thank you very much.